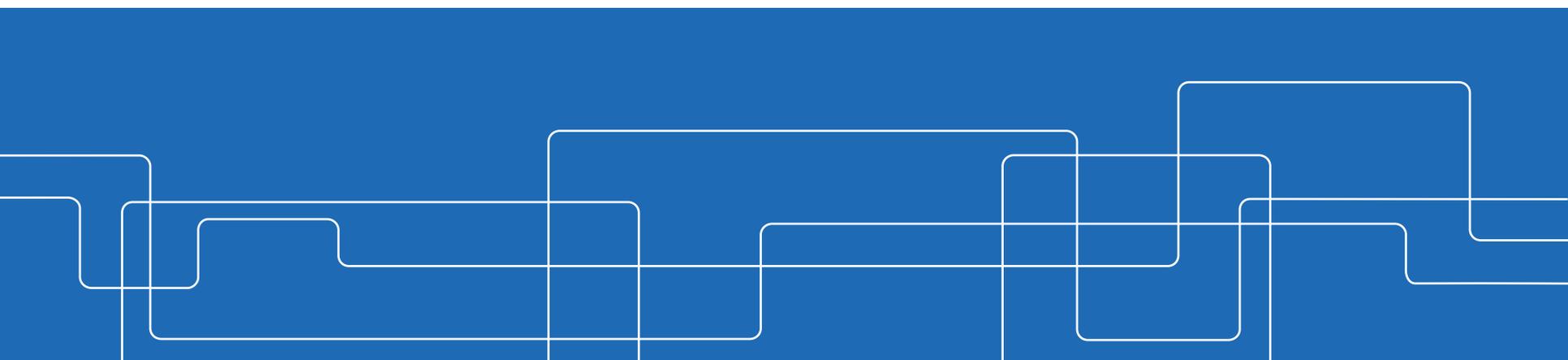


On Gas Dynamics of Exhaust Valves

Marcus Winroth, Christopher Ford, Henrik Alfredsson, Ramis Örlü
07.09.2017, CCGEx – Research Day

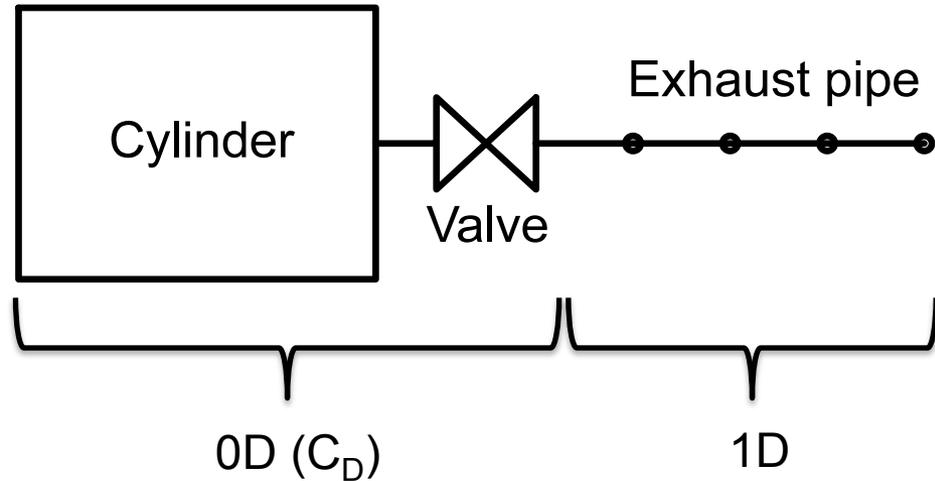
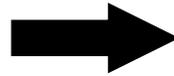
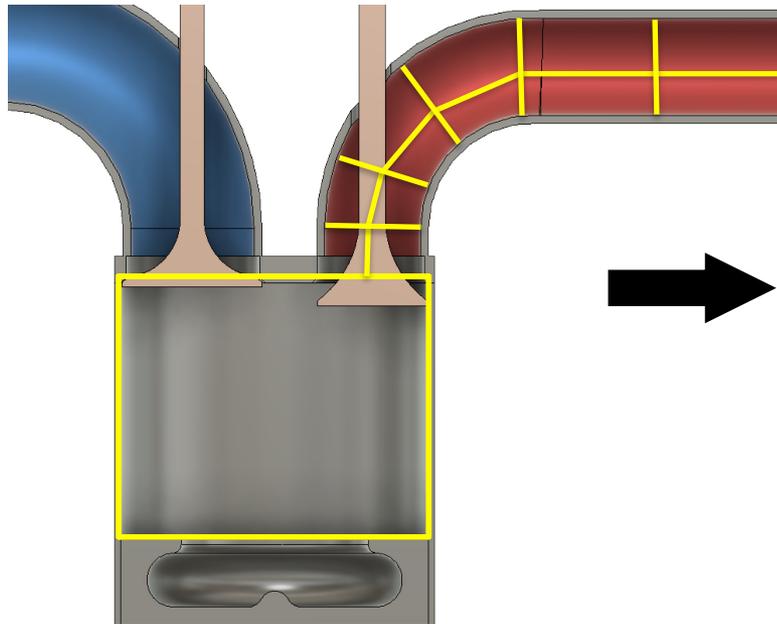


VOLVO



BorgWarner

1D/0D simulations



$$C_D = \frac{\dot{m}_{actual}}{\dot{m}_{ideal}}$$

Measurements of C_D today assume:

- Static valve (quasi-steady)
- Low pressure ratios (insensitive to pressure ratio)



Objectives



Experimentally investigate the effects on C_D due to:

- Engine speed (valve opening time)
- Pressure ratio

Ideal mass flow

$$C_D = \frac{\dot{m}_{actual}}{\dot{m}_{ideal}}$$

Subcritical:

$$\dot{m}_{ideal} = \frac{A_T p_0}{\sqrt{RT_0}} \left(\frac{p_T}{p_0} \right)^{\frac{1}{\gamma}} \left\{ \frac{2\gamma}{\gamma-1} \left[1 - \left(\frac{p_T}{p_0} \right)^{\frac{\gamma-1}{\gamma}} \right] \right\}^{\frac{1}{2}}$$

Choked:

$$\dot{m}_{ideal} = A_T p_0 \sqrt{\frac{\gamma}{RT_0}} \left(\frac{2}{\gamma+1} \right)^{(\gamma+1)/[2(\gamma-1)]}$$

A_T - Throat area

p_T - Throat pressure

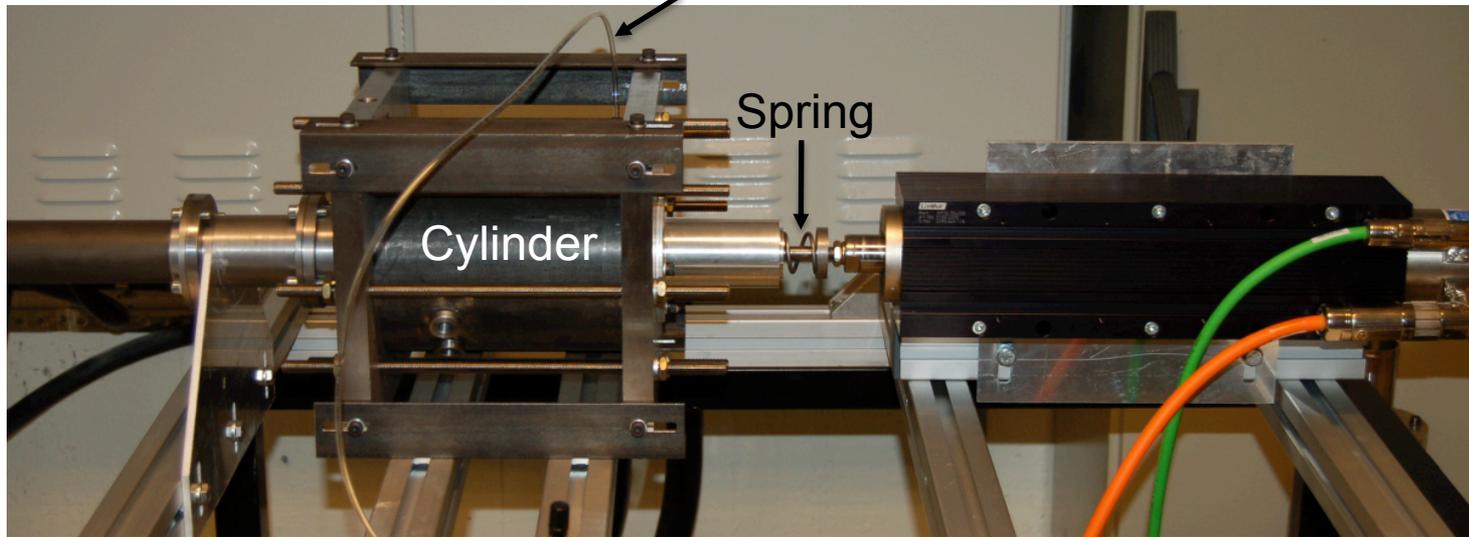
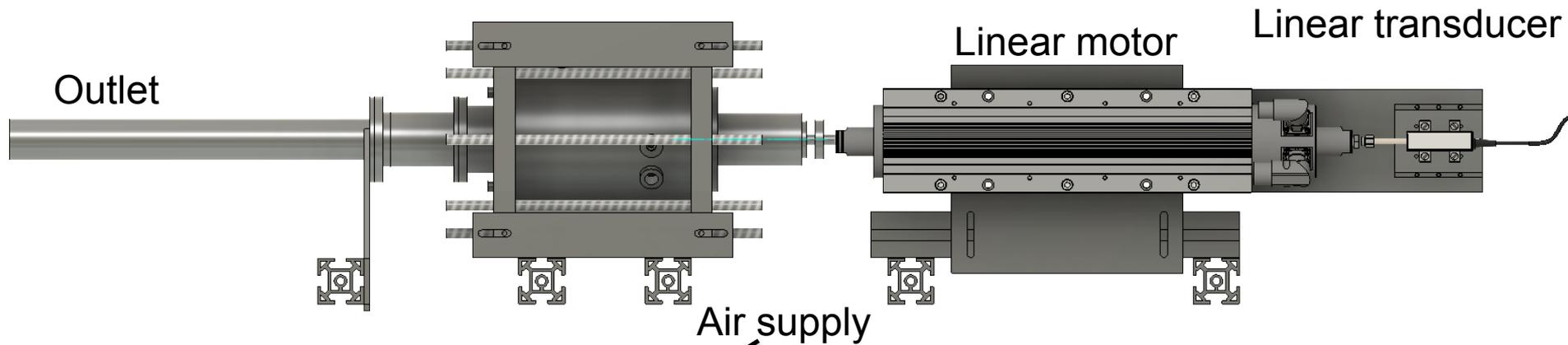
p_0 - Total pressure

T_0 - Total temperature

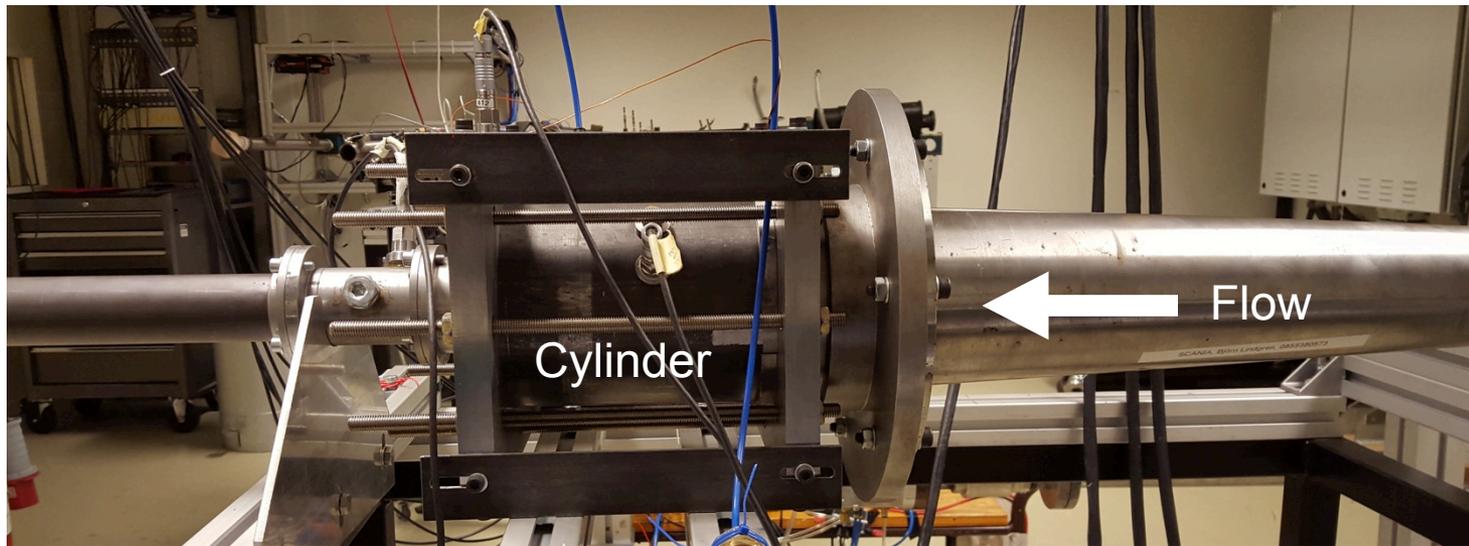
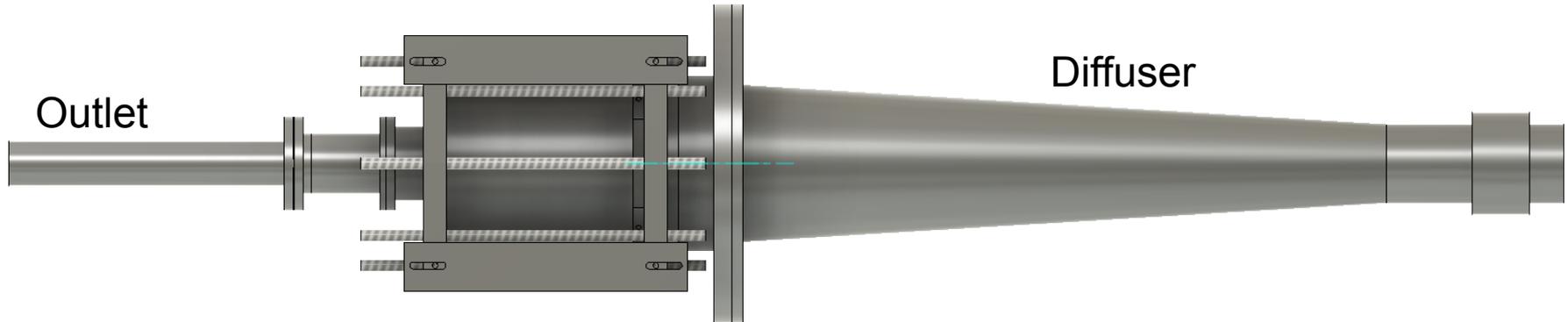
γ - Ratio of specific heats

R - Specific gas constant

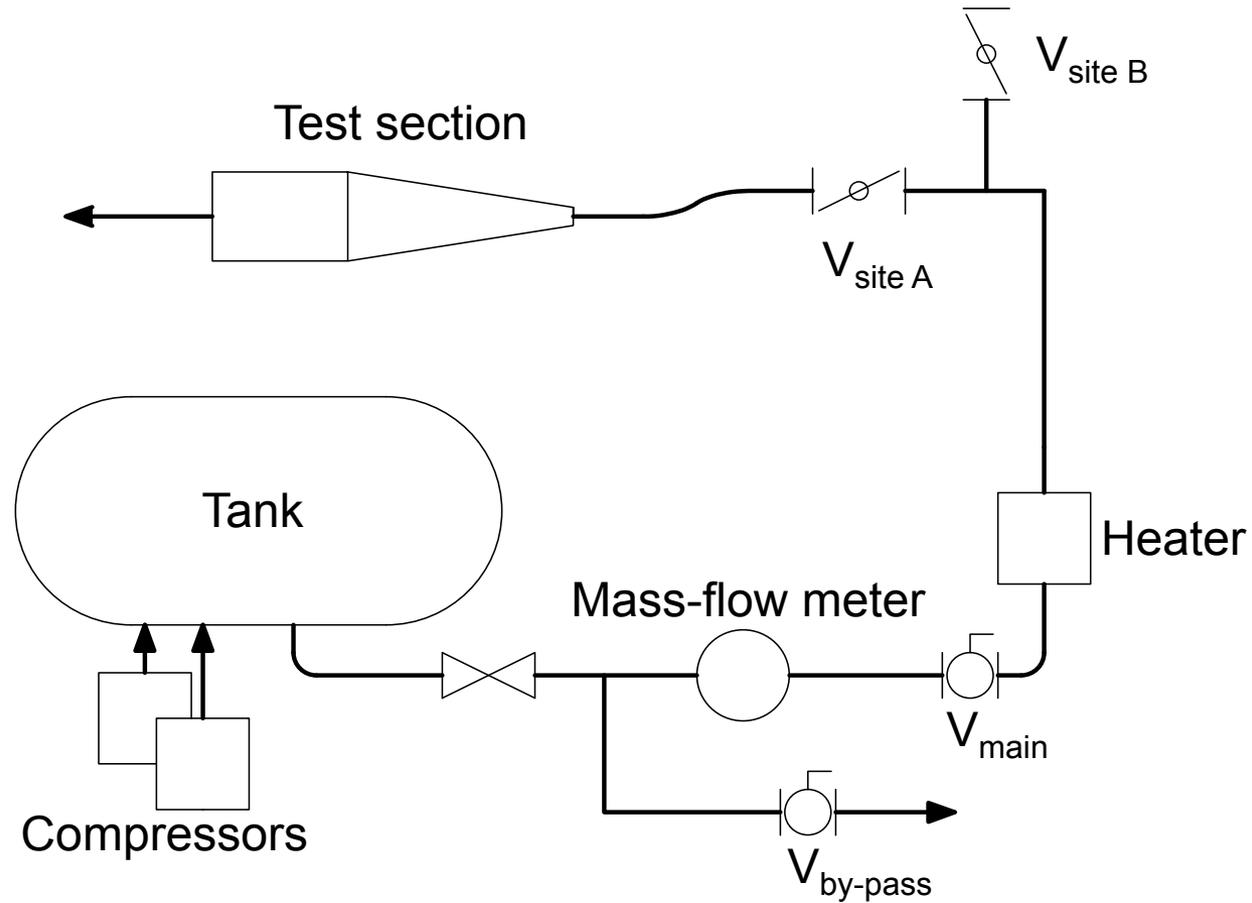
Dynamic valve setup



Static valve setup



$$\dot{m}_{max} = 0.5 \text{ kg/s}$$
$$p_{max} = 500 \text{ kPa}$$



Time-resolved mass flow

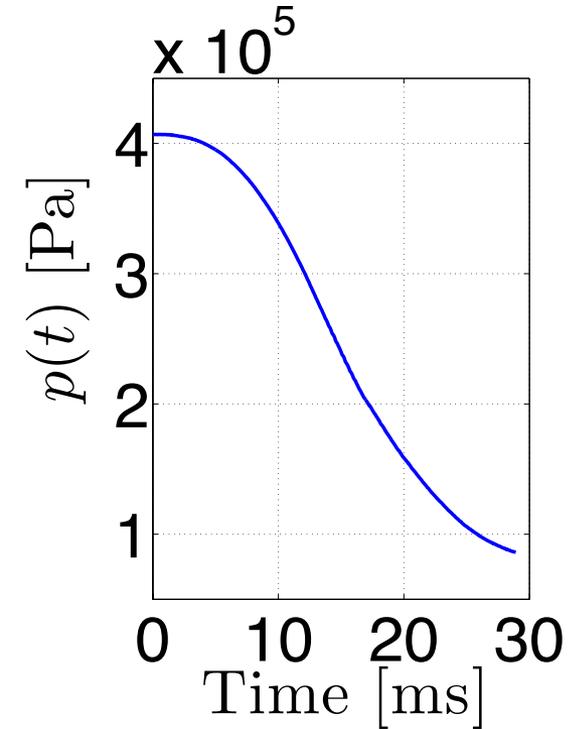
$$m(t) = \frac{V}{R} \frac{p(t)}{T(t)}$$

Expansion in the cylinder may be viewed as isentropic

$$\frac{p_2}{p_1} = \left(\frac{T_2}{T_1} \right)^{\gamma/(\gamma-1)}$$

Meaning the mass in the cylinder is a function of the pressure and initial temperature

$$m(t) = f(p(t), T(t = 0))$$

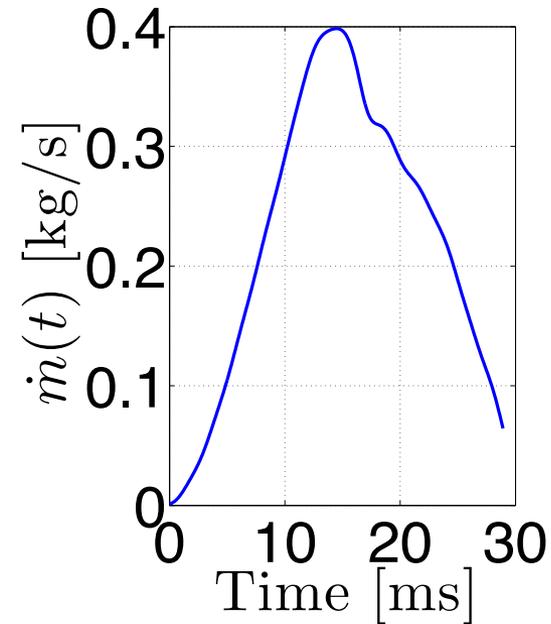
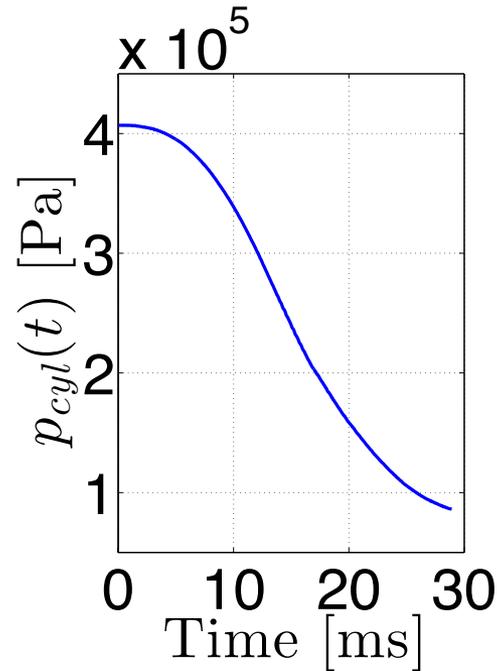


Time-resolved mass flow

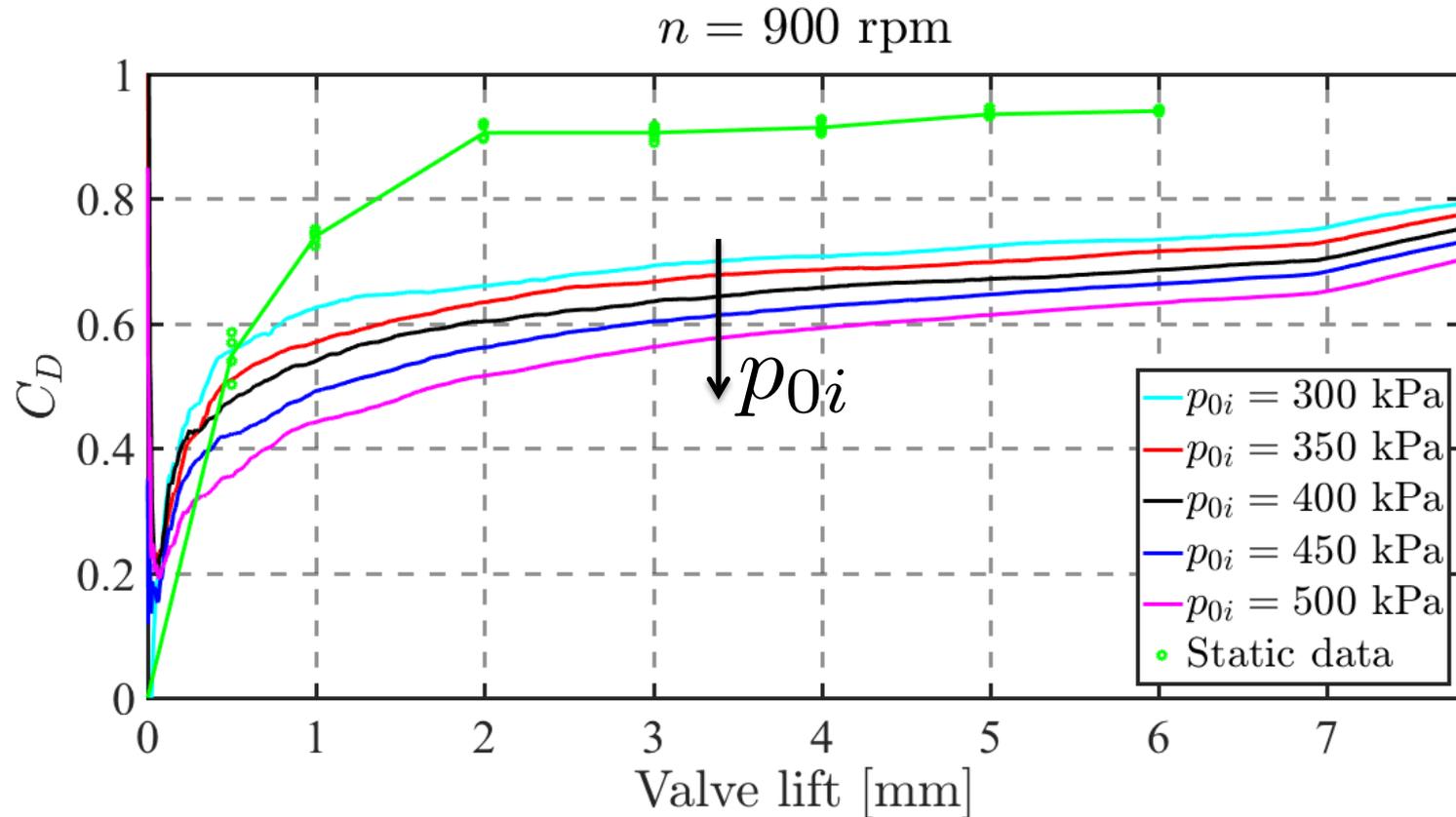
$$\dot{m} = \frac{dm}{dt} = \frac{V}{\gamma RT_{0i}} \left(\frac{p_{0i}}{p} \right)^{(\gamma-1)/\gamma} \frac{dp}{dt}$$

$n = 900$ rpm

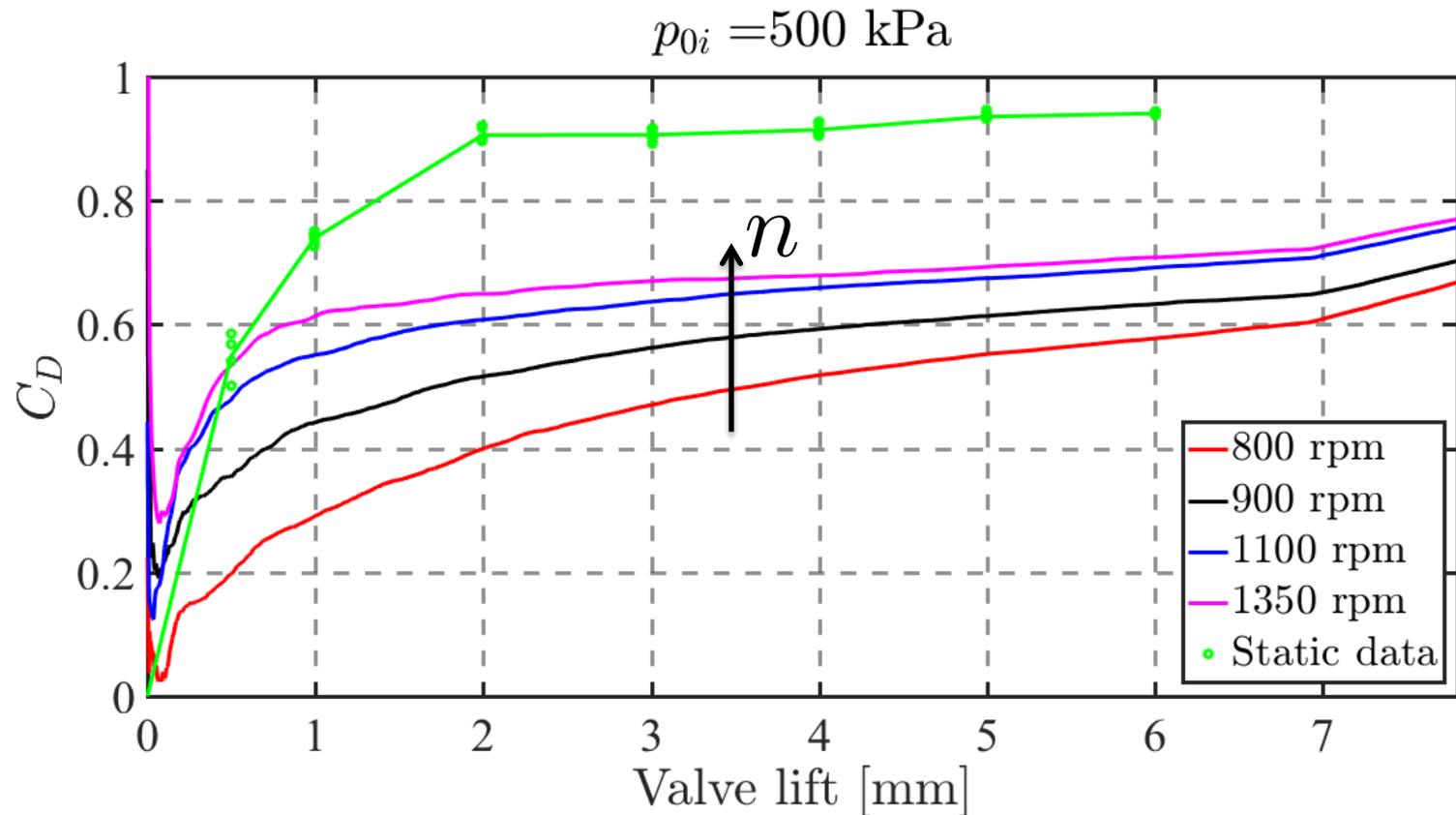
$p_{0i} = 400$ kPa



Initial pressure



Engine speed



Quasi-steadiness

$$u_{geometry} \ll u_{flow}$$

$$\tau_{geometry} \gg \tau_{flow} \Rightarrow \text{Quasi-steady}$$

Classical idea

Quasi-steadiness

$$u_{geometry} \ll u_{flow}$$

$$\tau_{geometry} \gg \tau_{flow} \Rightarrow \text{Quasi-steady}$$

Classical idea

Neglects the dynamics of the flow conditions

$$\tau_{condition} \gg \tau_{geometry} \gg \tau_{flow} \Rightarrow \text{Quasi-steady}$$

A measure of quasi-steadiness

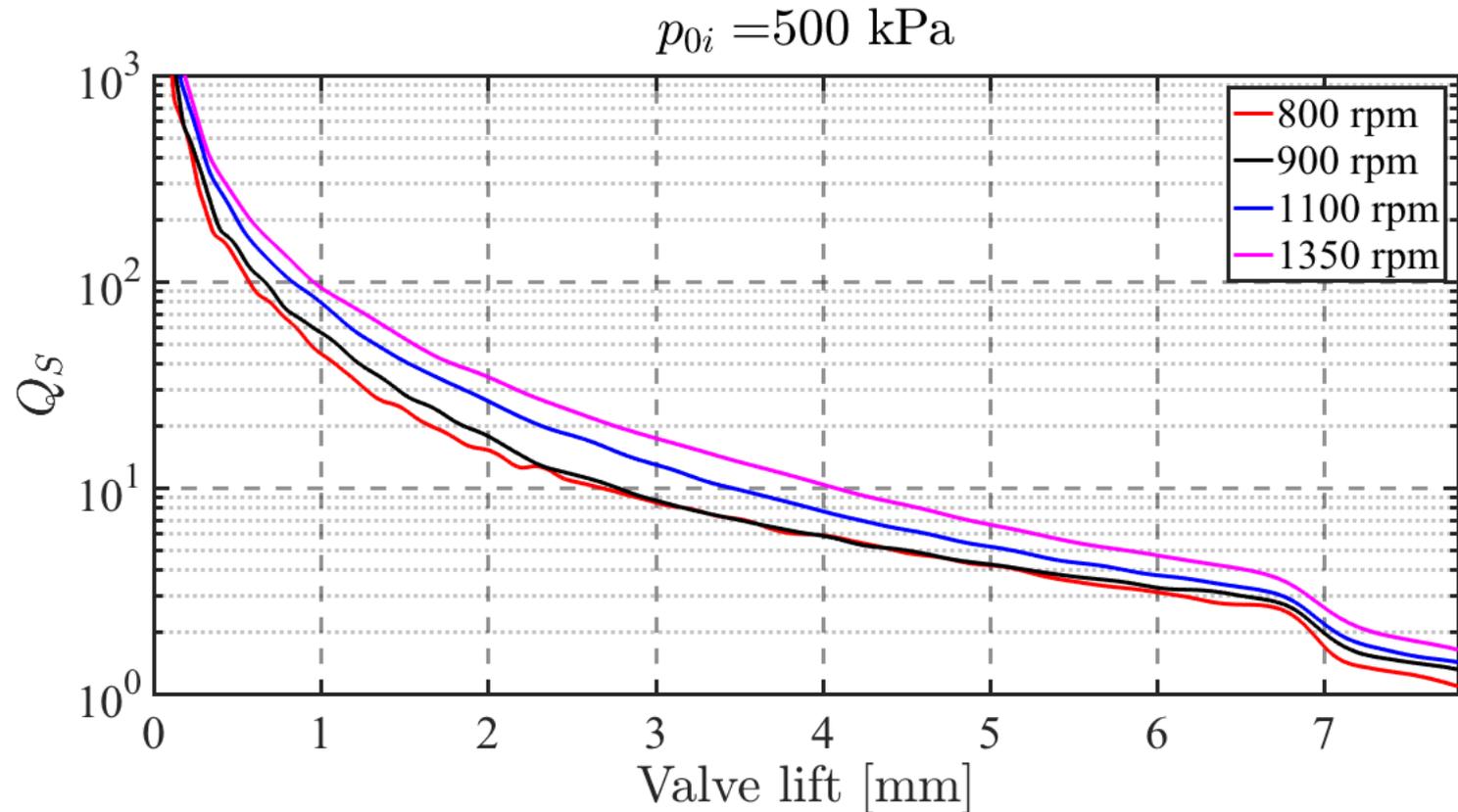
$$Q_S = \frac{\dot{A}_T / A_T}{\dot{m} / m}$$

$$Q_S = C \cdot \left(\frac{p_{0_i}}{p_0} \right)^{(\gamma-1)/2\gamma} \frac{V}{A_T \sqrt{\gamma R T_{0_i}}} \frac{\dot{A}_T}{A_T}$$

$Q_S \gg 1 \Rightarrow$ Quasi-steady

$$C = \left(\frac{\gamma + 1}{2} \right)^{(\gamma+1)/[2(\gamma-1)]}$$

A measure of quasi-steadiness





Conclusions



It has been shown that:

- ❑ The assumptions of quasi-steadiness and pressure-ratio independence do not hold
 - ❑ C_D decreases with initial pressure
 - ❑ C_D increases with engine speed

Reference:

M Winroth (2017) “On Gas Dynamics of Exhaust Valves”. Licentiate Thesis, KTH Mechanics, March 2017



Competence Center for Gas Exchange



”Charging for the future”

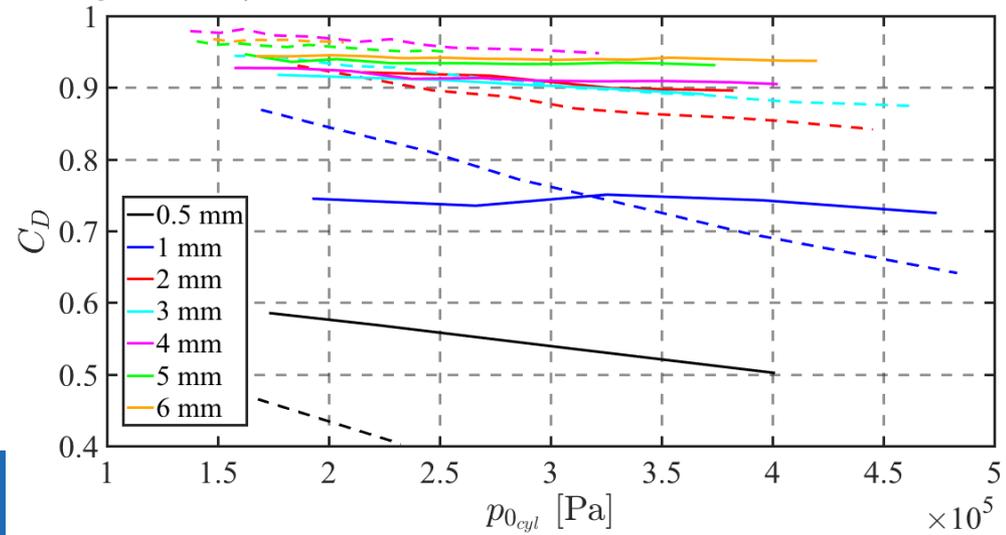
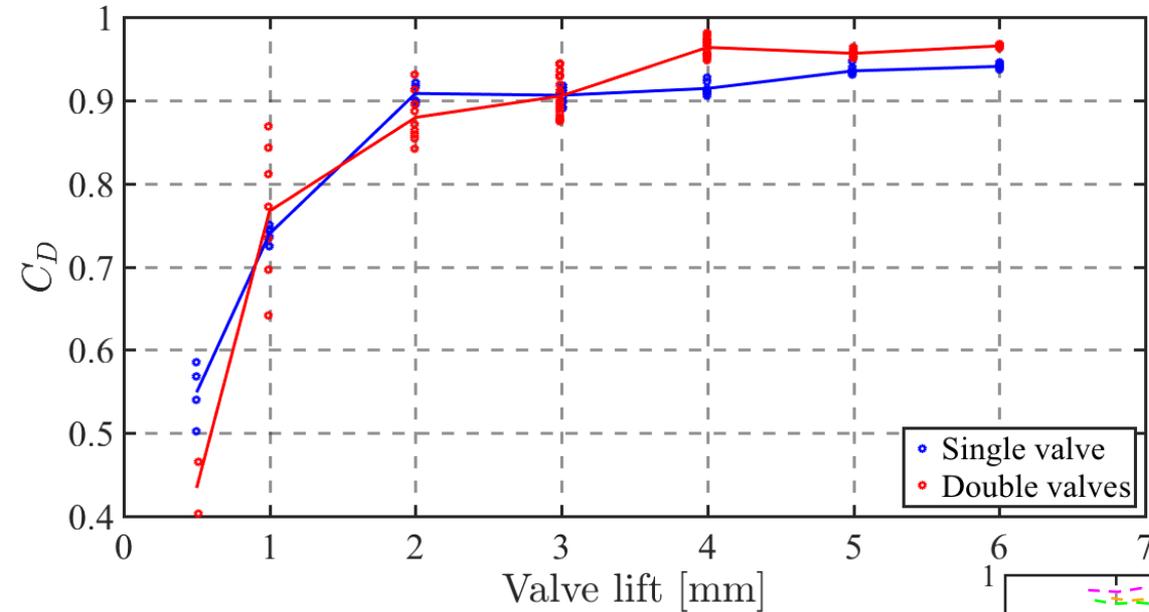


VOLVO

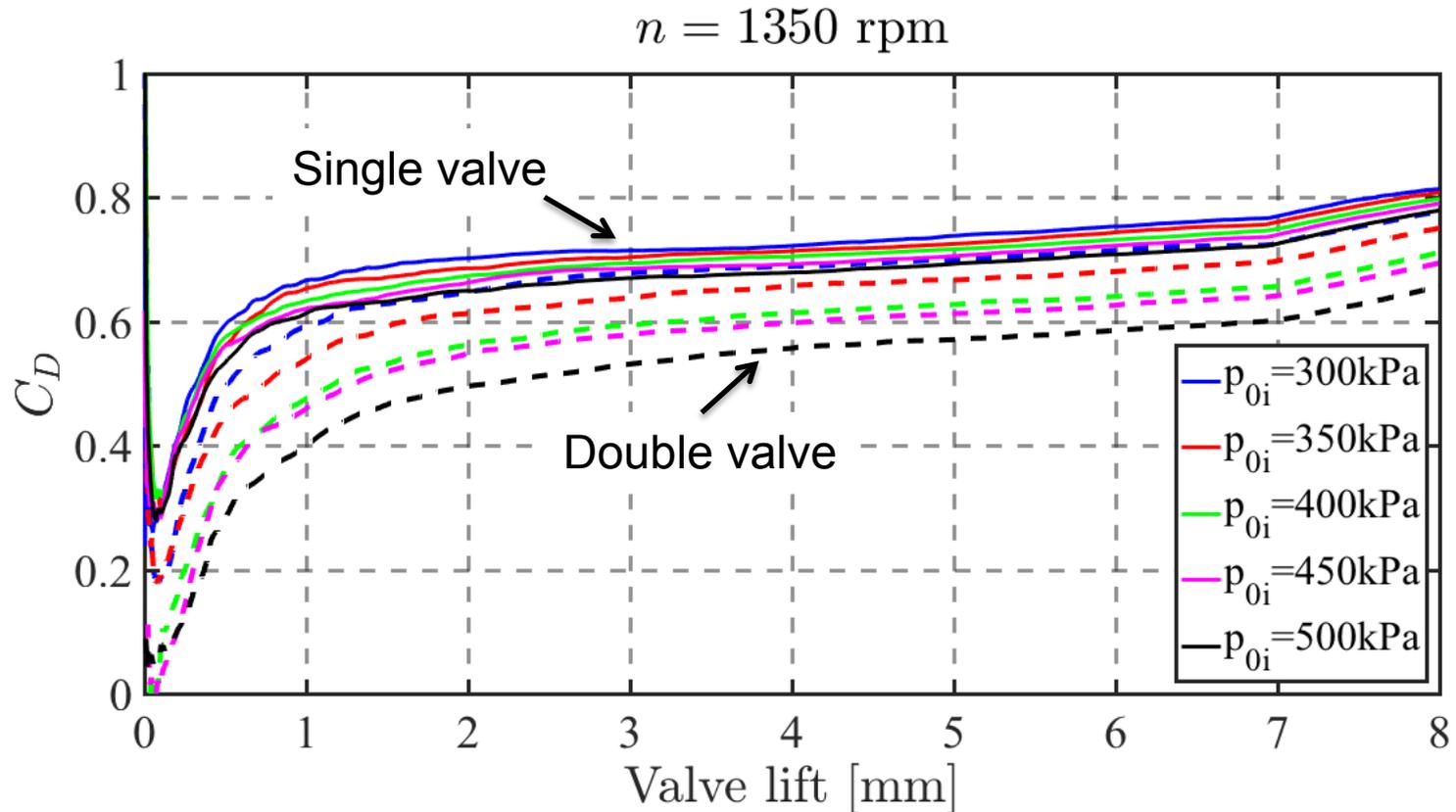


BorgWarner

Double-valve setup



Double-valve setup



Double-valve setup

