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Gas Dynamics of Exhaust Valves

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Outline

- Background and objectives
- Experimental setup and techniques
- Early results and conclusions



Background

- Semi empirical 1D models used for optimization of engine system

- Discharge coefficient

$$C_D = \frac{\dot{m}_{real}}{\dot{m}_{actual}}$$

- Measurements of C_D today:
 - Fixed valve lift (assuming quasi steady)
 - Low pressure ratios (assuming pressure ratio independence)
 - Typical experiments performed in industry have a maximum $M \approx 0.3$ (incompressible)



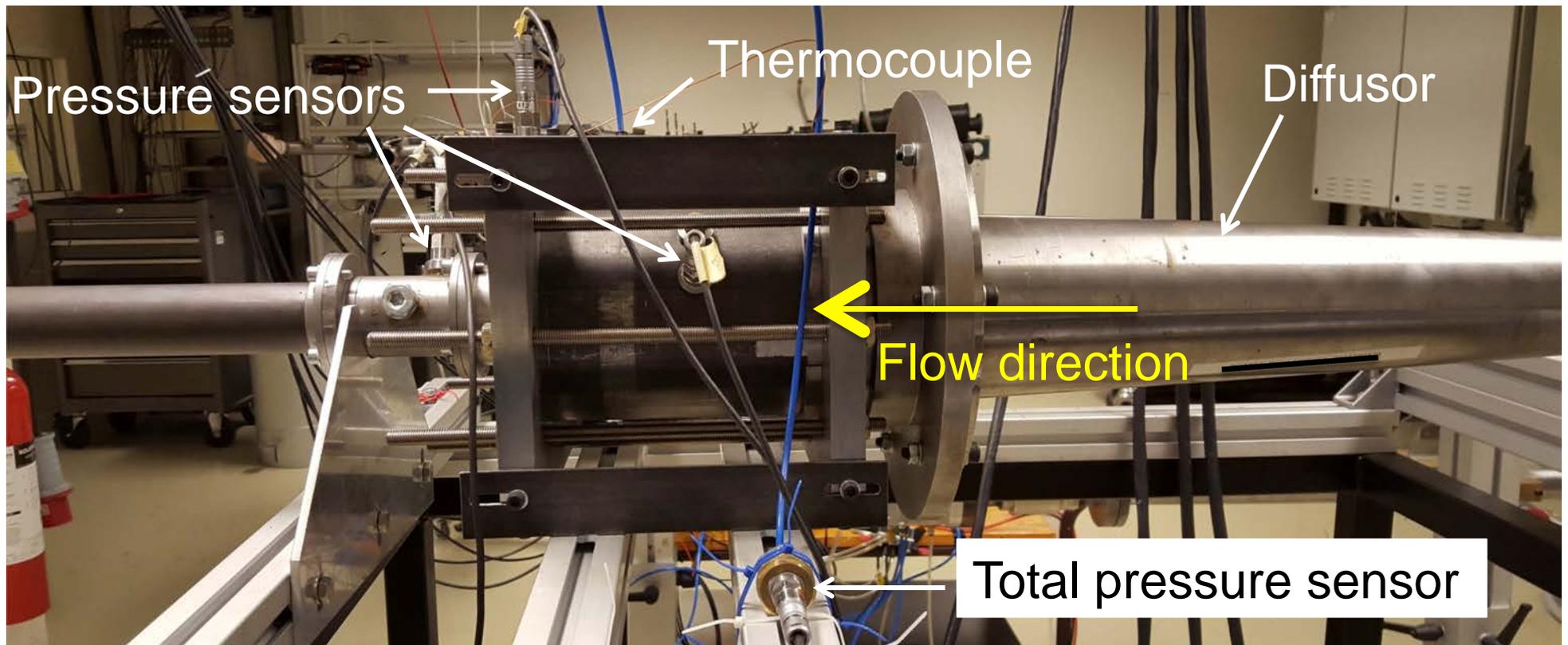
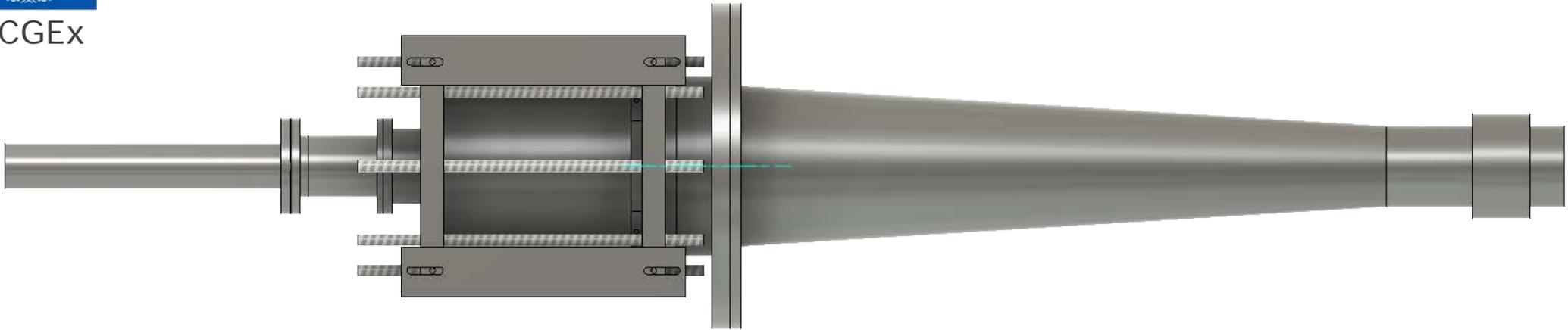
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Objectives

Experimentally test the effects of:

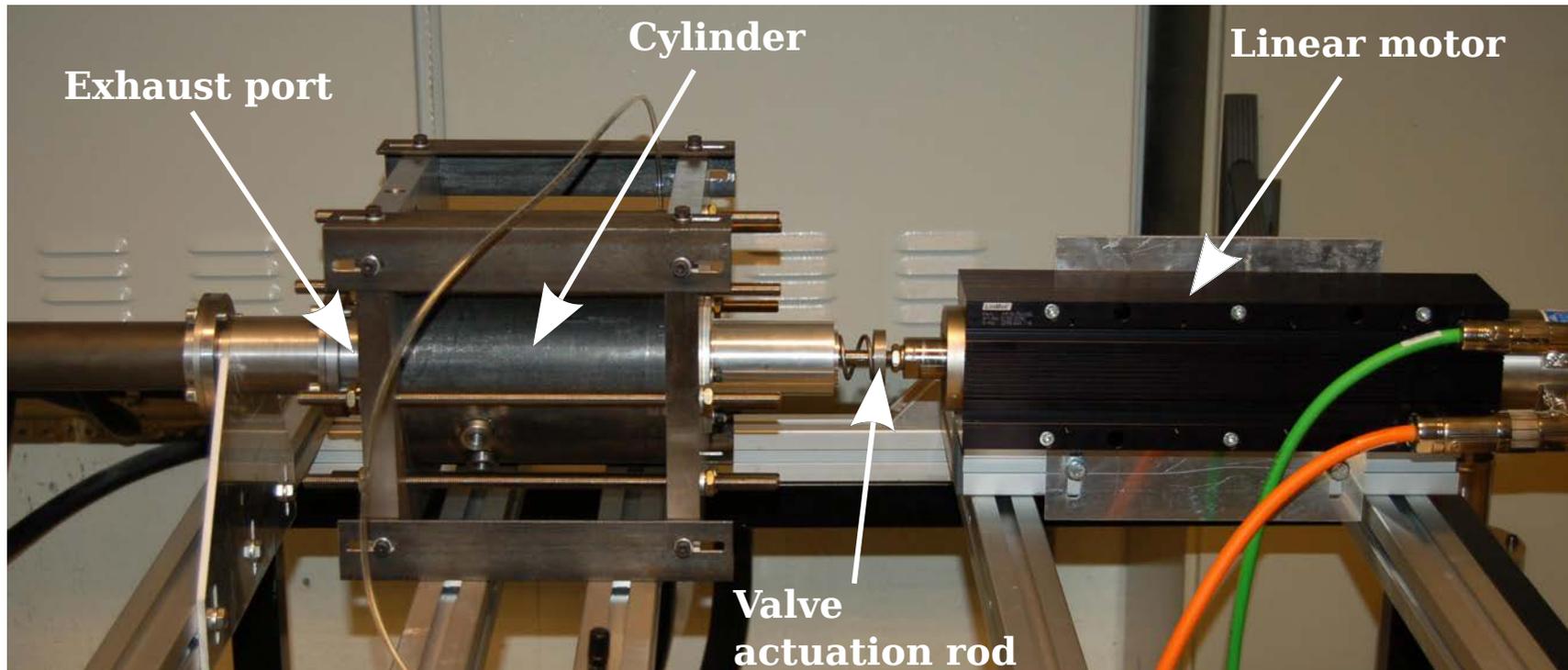
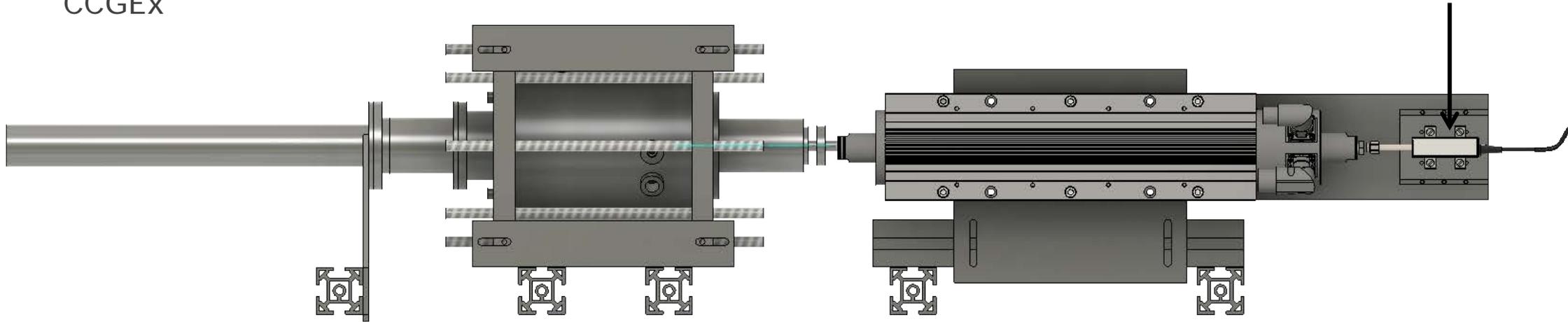
- Quasi-steady valve assumption
- High pressure ratio
- Radial positioning of the valve
- Interaction of two valves
- Valve opening profiles
- Exhaust port geometry

Static valve setup

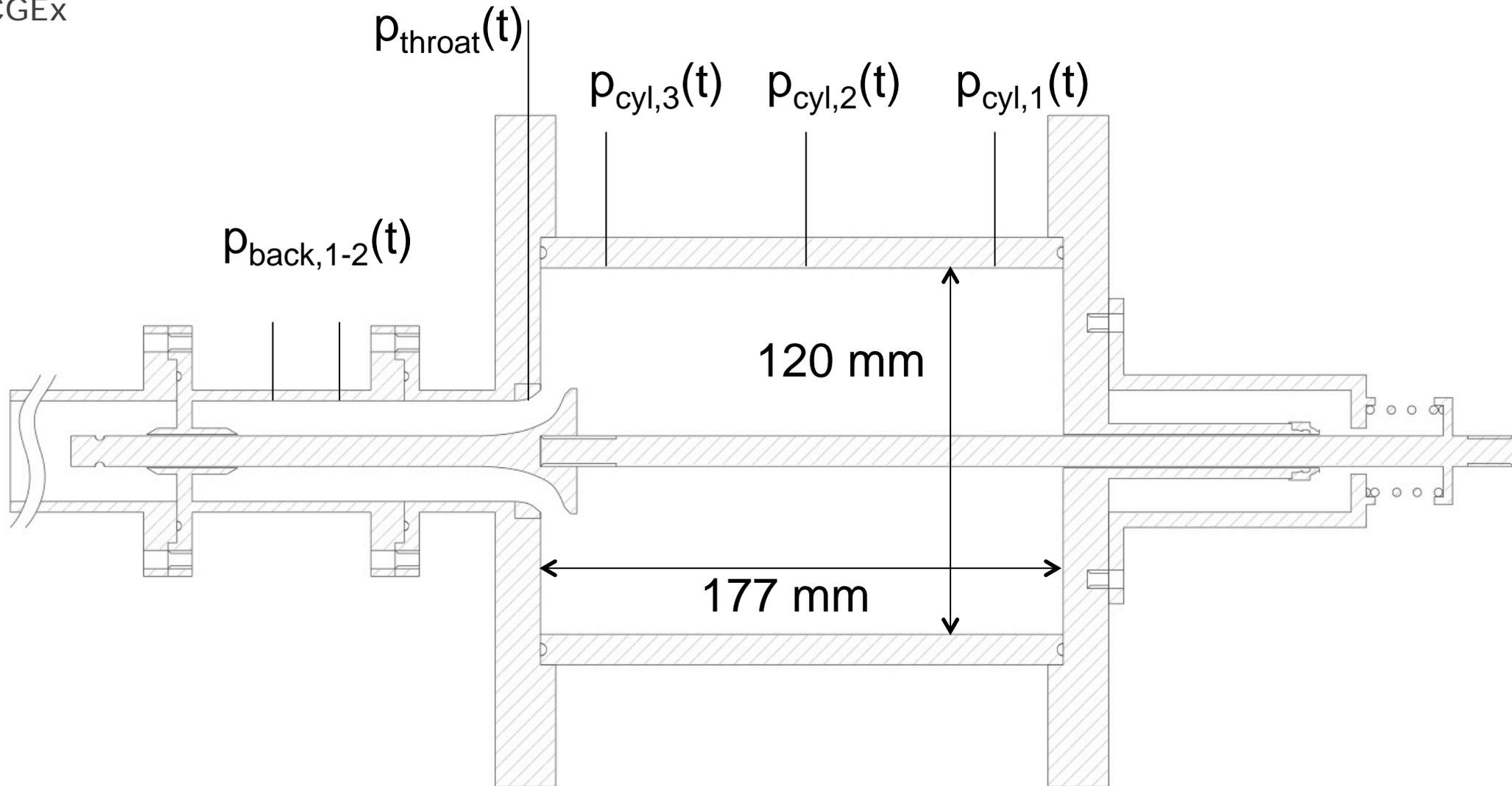


Dynamic valve setup

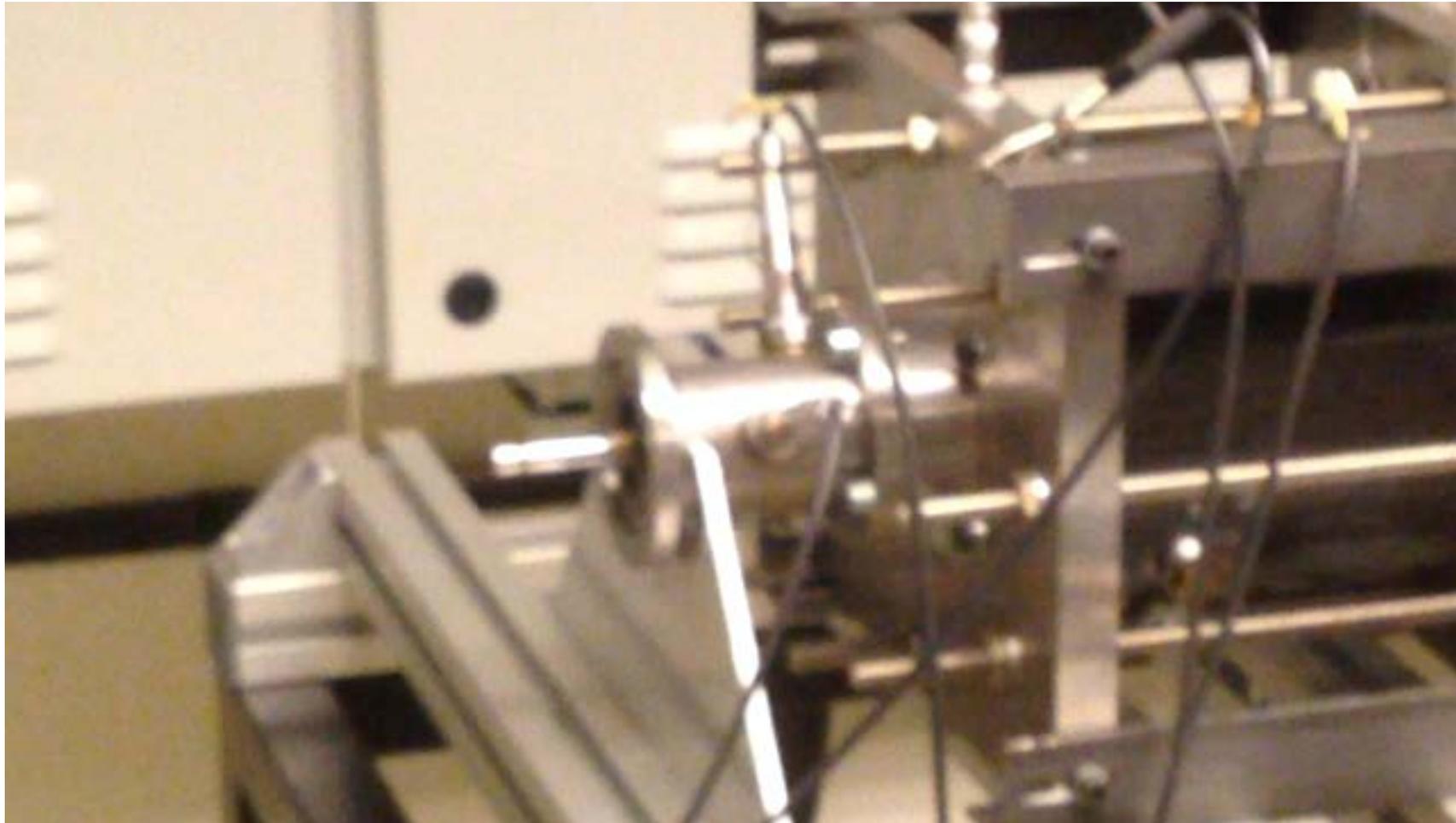
Linear transducer



Dynamic valve setup



Dynamic valve setup





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C_D

$$C_D = \frac{\dot{m}_{actual}}{\dot{m}_{ideal}}$$

Using the isentropic relations, the Mach number and conservation of mass flow gives for sub-critical flows:

$$\dot{m}_{ideal} = \frac{A_T p_0}{\sqrt{RT_0}} \left(\frac{p_T}{p_0} \right)^{\frac{1}{\gamma}} \left\{ \frac{2\gamma}{\gamma - 1} \left[1 - \left(\frac{p_T}{p_0} \right)^{\frac{\gamma-1}{\gamma}} \right] \right\}^{\frac{1}{2}}$$

A_T – Throat area

p_T – Throat pressure

p_0 – Cylinder total pressure

γ – Ratio of specific heats

R – Specific gas constant

C_D

$$C_D = \frac{\dot{m}_{actual}}{\dot{m}_{ideal}}$$

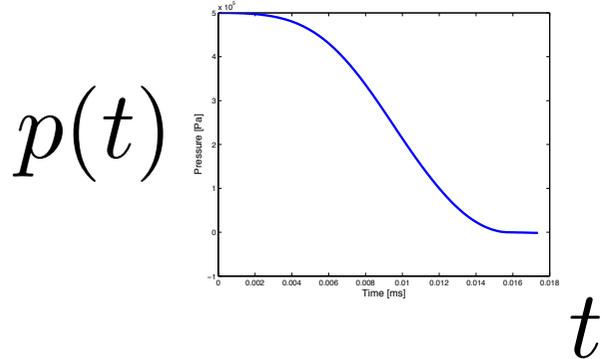
Using the isentropic relations, the Mach number and conservation of mass flow gives for sub-critical flows:

$$\dot{m}_{ideal} = \frac{A_T p_0}{\sqrt{RT_0}} \left(\frac{p_T}{p_0} \right)^{\frac{1}{\gamma}} \left\{ \frac{2\gamma}{\gamma - 1} \left[1 - \left(\frac{p_T}{p_0} \right)^{\frac{\gamma-1}{\gamma}} \right] \right\}^{\frac{1}{2}}$$

While for choked conditions:

$$\dot{m}_{ideal} = \frac{A_T p_0}{\sqrt{RT_0}} \gamma^{1/2} \left(\frac{2}{\gamma + 1} \right)^{\frac{\gamma+1}{2(\gamma-1)}}$$

Time resolved mass flow



$$m(t) = \frac{V}{R} \frac{p(t)}{T(t)}$$

The expansion in the cylinder may be viewed as isentropic, hence

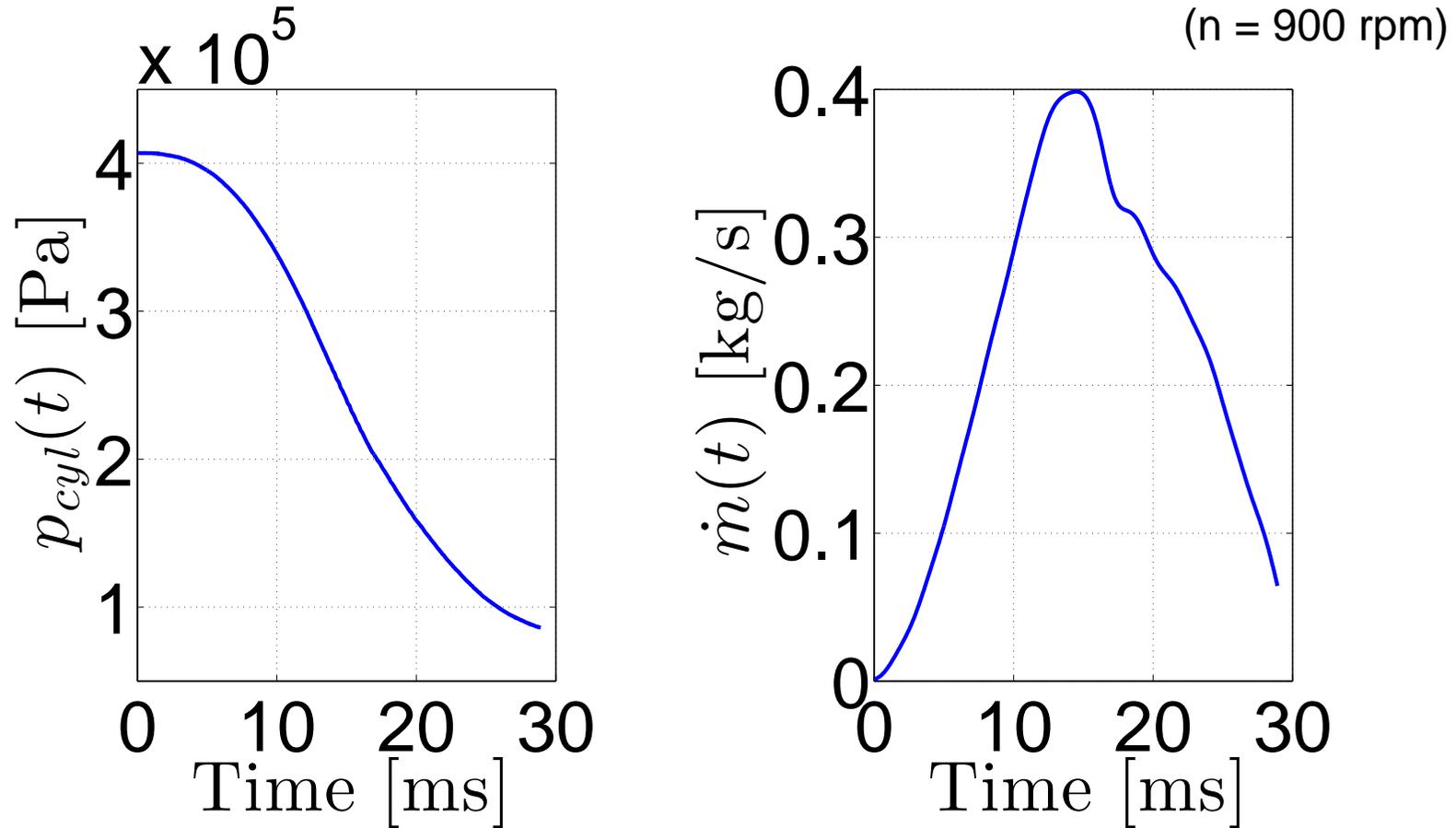
$$\frac{p}{p_0} = \left(\frac{T}{T_0} \right)^{\gamma/(\gamma-1)}$$

which gives

$$\frac{p}{T} = T_0^{-1} p_0^{(\gamma-1)/\gamma} p^{1/\gamma} = C p^{1/\gamma}$$

Meaning it is sufficient to measure $p(t)$ and $T(t=0)$ to obtain the mass flow.

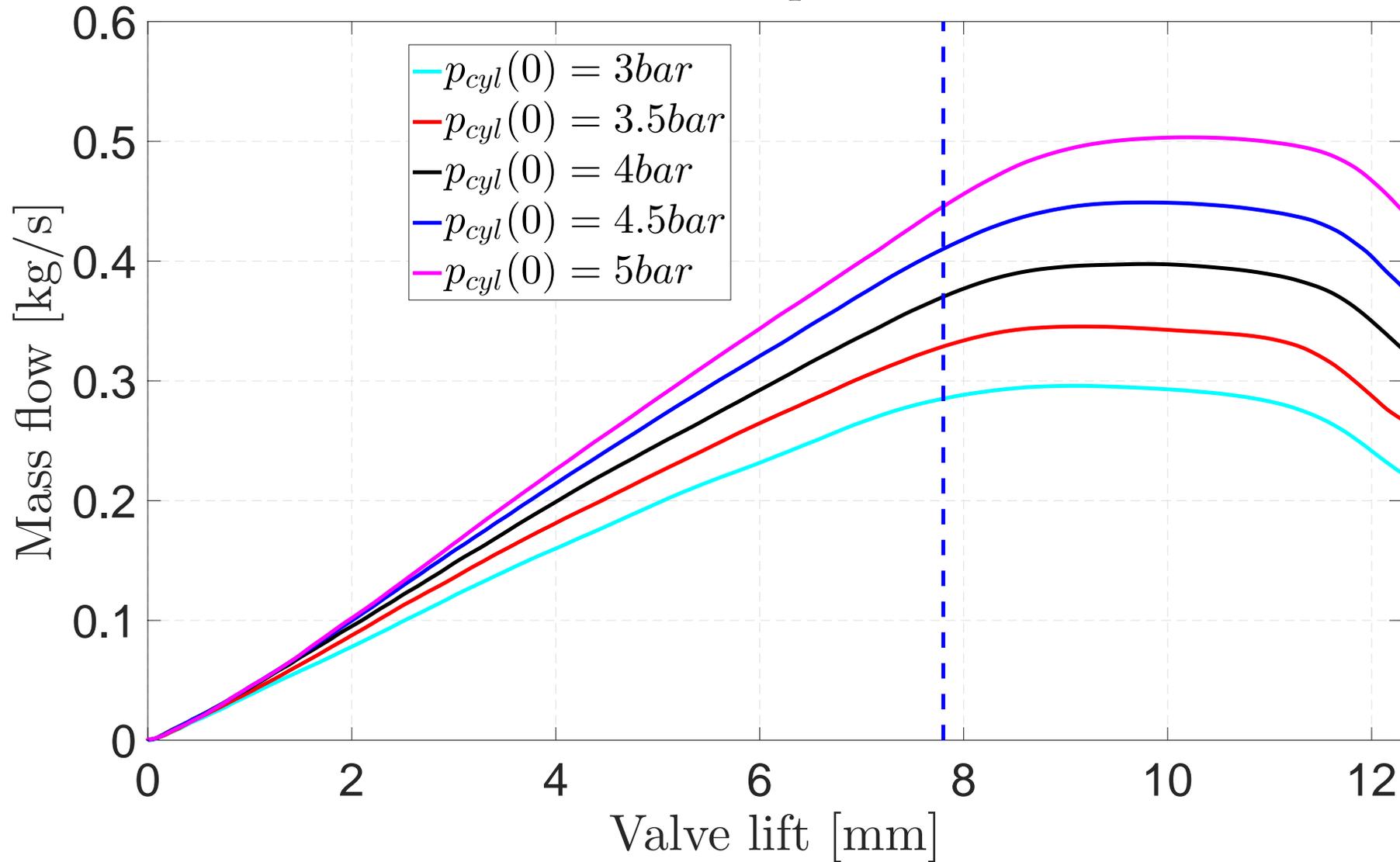
Time resolved mass flow



$$\dot{m} = \frac{dm}{dt} = \frac{V}{\gamma RT_0} \left(\frac{p_0}{p} \right)^{(\gamma-1)/\gamma} \frac{dp}{dt}$$

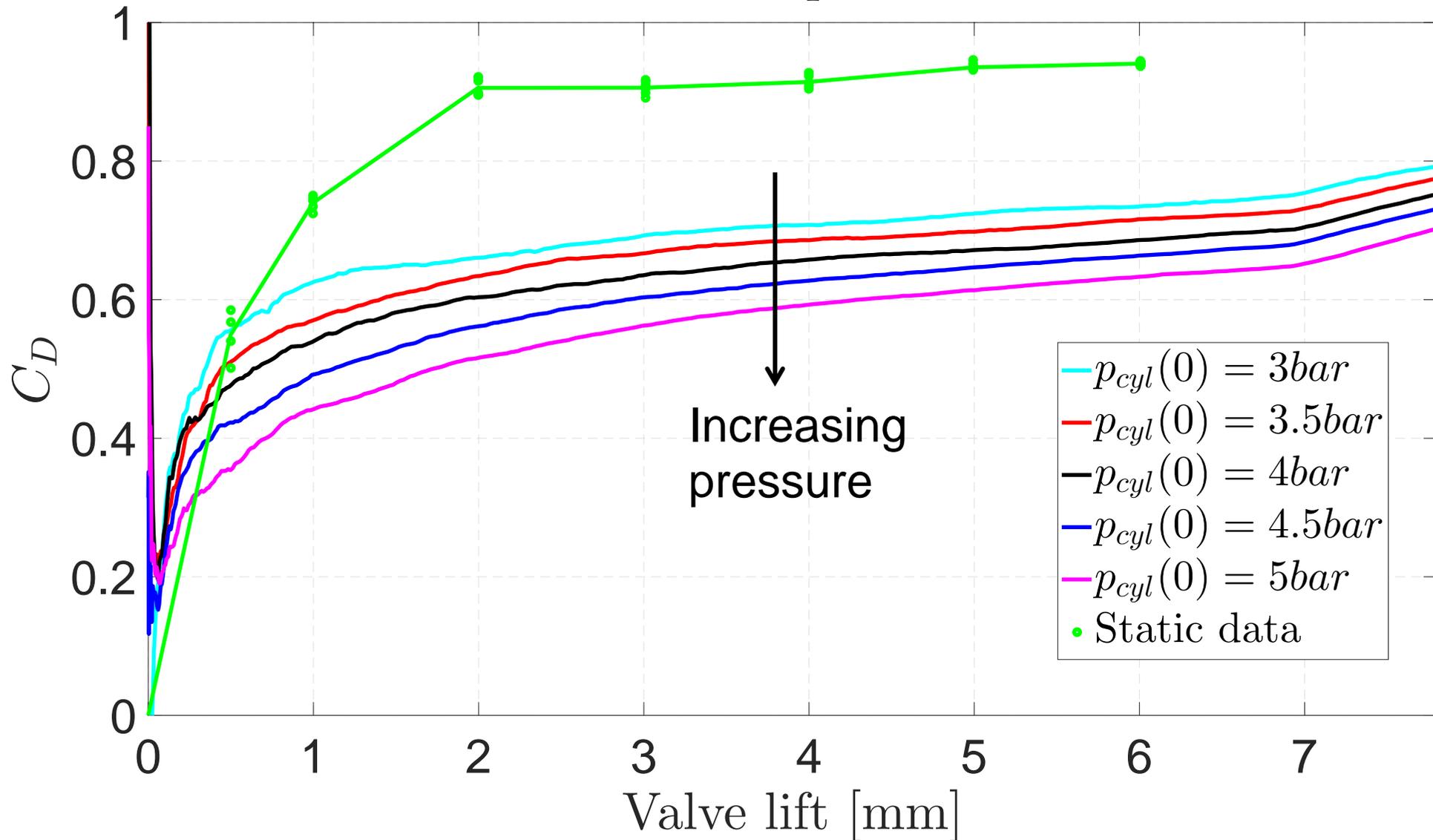
Mass flow @ 900 rpm

900rpm



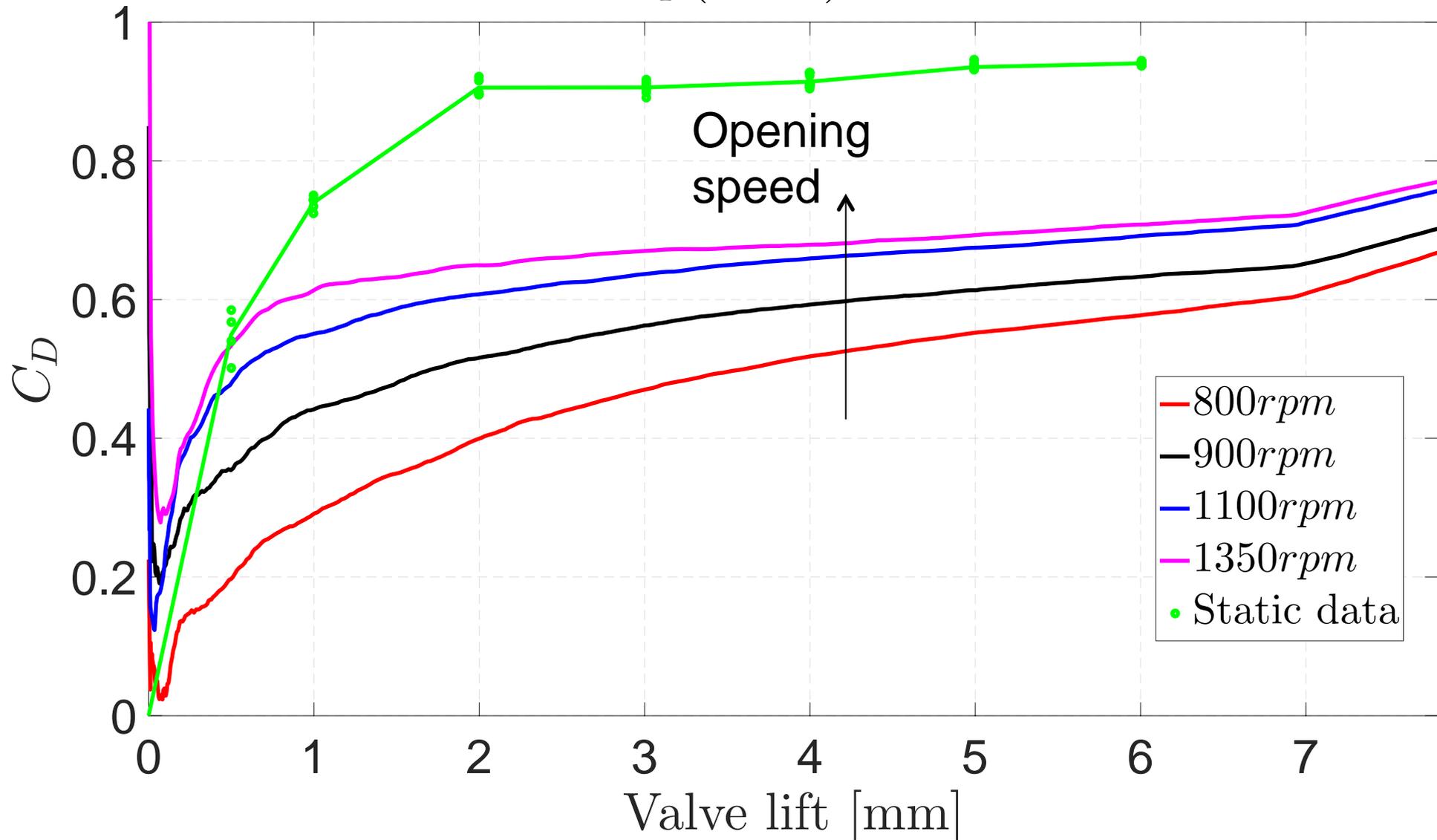
C_D @ 900 rpm

900rpm



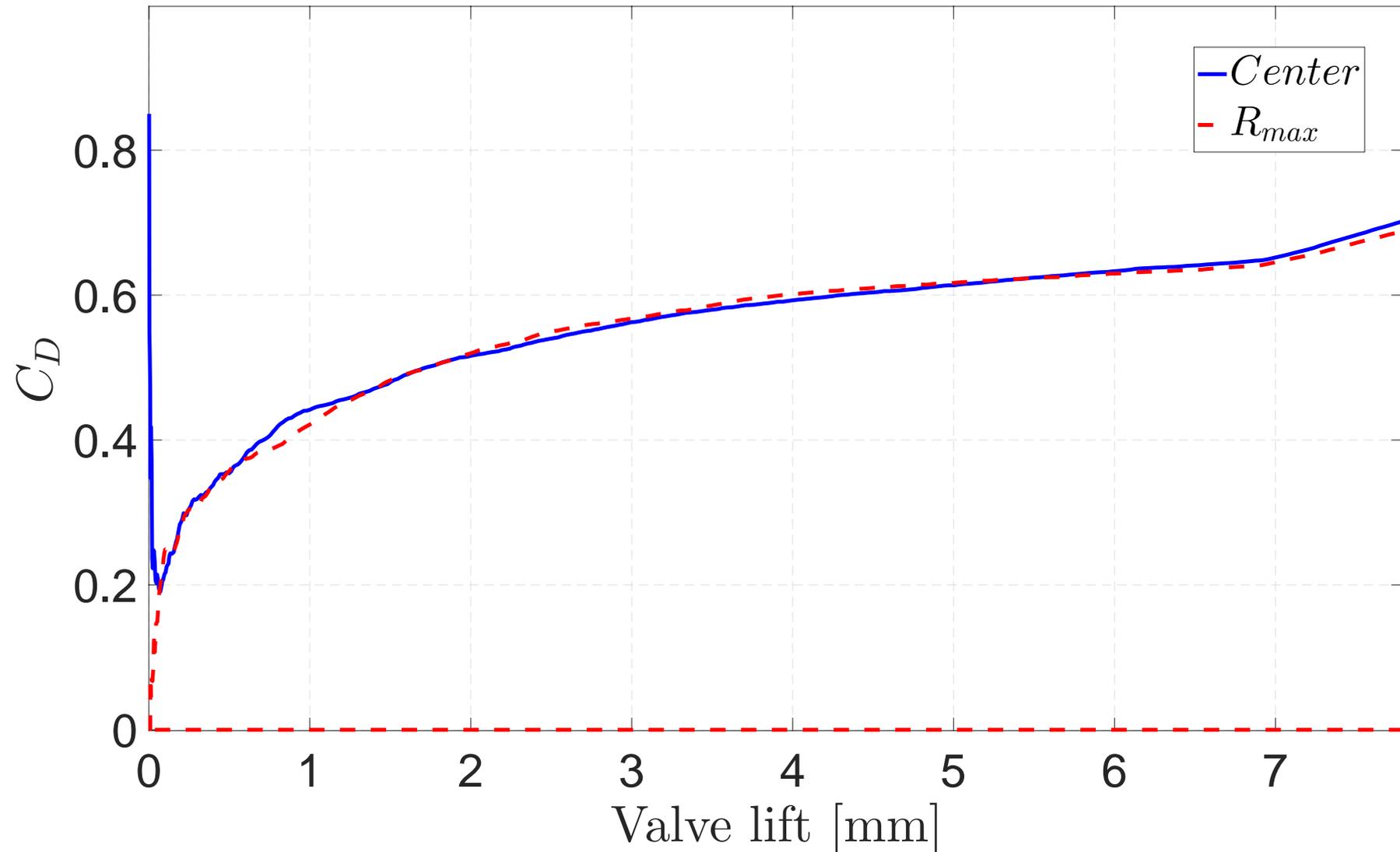
$C_D @ p(0) = 5\text{bar}$

$$p(t = 0) = 5$$



Radial position

Different R @ $p_{cyl}(0) = 5bar$





Initial conclusions

- Assumption of pressure ratio independence:
 - Increasing the pressure ratio decreases the C_D -value
 - The static measurements of C_D seems relatively insensitive to pressure ratio
- The quasi-steady assumption:
 - Strong temporal effects
 - Faster opening leads to a higher C_D
 - Faster opening leads to a faster increase C_D
 - Static measurements over predicts the value of C_D
- C_D appears to be insensitive to radial position of the valve

Future work

- Test the effect of:
 - double valve combination (on going)
 - different valve opening profiles
 - different exhaust pipe geometries





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Thank you for your attention!



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